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### Theoretical framework

Comment on the notation used in classical textbooks

### Constructive procedure

Construction of a pseudo-potential

Drucker-Prager model

Non-linear Kinematic Hardening (NLK)

Endochronic theory

Conclusion

## Constitutive laws for plasticity

 $\mathbb{E} = \{\mathbf{x} \in \mathbb{V} \ / \ f(\mathbf{x}) \le 0\} \text{ elastic domain}$ for the generalized thermodynamic forces  $\mathbf{x} \in \mathbb{V}$ 

1. Associative flow rules

generalized normality condition of the flow  $\mathbf{x}^* \in \mathbb{V}^*$  to the boundary of  $\mathbb{E}$ , (Halphen, Nguyen)

 Non-associative flow rules the direction of the flow x\* is defined as the gradient of the plastic potential g(x).

 $\implies$  introduction of pseudo-potentials to make sure that the mechanical dissipation is positive (Moreau ).

## Associative flow rules

Definition of pseudo-potentials x generalized thermodynamic force , x\* flow.

$$\begin{split} \phi(\mathbf{x}) &:= \mathbb{I}_{\mathbb{E}}(\mathbf{x}) & \text{indicator function of the elastic domain} \mathbb{E} \\ \phi^*(\mathbf{x}^*) &:= \sup_{\mathbf{x} \in \mathbb{V}} (\mathbf{x} \cdot \mathbf{x}^* - \phi(\mathbf{x})) & \text{the Legendre-Fenchel conjugate of } \phi \\ \forall \ (\mathbf{x}, \mathbf{x}^*) \in \mathbb{V} \times \mathbb{V}^* & \phi(\mathbf{x}) + \phi^*(\mathbf{x}^*) \geq \mathbf{x} \cdot \mathbf{x}^* \end{split}$$

The equality is reached for a pair  $(\mathbf{\tilde{x}}, \mathbf{\tilde{x}}^*)$  which verifies

 $\mathbf{\tilde{x}}^* \in \partial \phi(\mathbf{\tilde{x}})$  and  $\mathbf{\tilde{x}} \in \partial \phi^*(\mathbf{\tilde{x}}^*)$ 

and  $(\tilde{\mathbf{x}}, \tilde{\mathbf{x}}^*)$  are the real physical values.

For non-associative flow rule the definition of such pseudo-potentials is not straightforward.

## Non-associative flow rule

Two different approaches :

 Introduction of a bipotential (de Saxcé, Hjiaj, Bodovillé) b(x,x\*) depending on the dual variables, the thermodynamic force x and the flow x\*, separately convex and such that :

 $\forall (\mathbf{x}, \mathbf{x}^*) \in \mathbb{V} imes \mathbb{V}^* \qquad b(\mathbf{x}, \mathbf{x}^*) \geq \mathbf{x} \cdot \mathbf{x}^*$ 

Introduced for Drucker-Prager model and unilateral contact.

The stress-strain evolution is defined by the extremal couples of the bipotential.

In the simple case of associative flow rule :

$$orall \left( {f x},{f x}^st 
ight) \in {\mathbb V} imes {\mathbb V}^st \qquad b({f x},{f x}^st) := \phi({f x}) + \phi^st ({f x}^st)$$

second approach :

## 2. Introduction of pseudo-potentials

depending on the state variables + Helmholtz free energy (Ziegler)

depending on generalized stresses + Gibbs free energy (Collins, Houlsby, Puzrin , etc)

several exemples : Drucker-Prager, non-linear kinematic hardening, endochronic theory, Mroz (Erlicher, Point)

Link between these two different approaches?

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Bipotential
and/or
conjugated pseudo-potentials
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## General theoretical framework and notations

Assumption : isothermal and infinitesimal transformations.  $\mathbf{f}^{nd} \in \mathbb{V}$  non-dissipative (quasi-conservative) thermodynamic forces defined as the gradient of the Helmholtz free density of energy  $\psi(\mathbf{v})$ 

$$\mathbf{f}^{nd} = \nabla \psi \left( \mathbf{v} \right) \tag{1}$$

 $\Phi_m$  mechanical dissipation  $\Phi_m(t) := \mathbf{f} : \dot{\mathbf{v}} - \dot{\psi} = \mathbf{f} : \dot{\mathbf{v}} - \mathbf{f}^{nd} \cdot \dot{\mathbf{v}}$ **f** external forces,  $\mathbf{f}^d$  dissipative thermodynamic forces defined by :

 $\mathbf{f}^d := \mathbf{f} - \mathbf{f}^{nd}$ 

2nd principle : the mechanical dissipation is assumed nonnegative :

$$\Phi_m(t) = (\mathbf{f} - \mathbf{f}^{nd}) \cdot \dot{\mathbf{v}} = \mathbf{f}^d \cdot \dot{\mathbf{v}} \ge 0$$
(2)

To define conjugate pseudo-potentials is a usual way to obtain (2) :

$$\mathbf{f}^{d} \in \partial \phi^{*}\left( \dot{\mathbf{v}} 
ight)$$
 and  $\dot{\mathbf{v}} \in \partial \phi\left( \mathbf{f}^{d} 
ight)$ 

For the state variables  $(\varepsilon, \mathbf{u}) = (\varepsilon, \varepsilon^{p}, \alpha)$  we use the distinction between

dissipative forces : 
$$\mathbf{f}^{d} = (\sigma^{d}, \mathbf{p}^{d}) = (\sigma^{d}, \tau^{d}, \mathbf{X}^{d})$$
  
non-dissipative forces :  $\mathbf{f}^{nd} = (\sigma^{nd}, \mathbf{p}^{nd}) = (\sigma^{nd}, \tau^{nd}, \mathbf{X}^{nd})$ 

 $\sigma^d$  and  $\sigma^{nd}$  are the thermodynamic forces associated with  $\varepsilon$ .  $\tau^d$  and  $\tau^{nd}$  are the thermodynamic forces associated with  $\varepsilon^p$ . If the dissipation is independent of  $\dot{\varepsilon}$  the corresponding actual value of the dissipative force must be  $0: \sigma^d = 0$ hence  $\sigma = \sigma^{nd}$ , often  $\sigma$  is written instead of  $\sigma^{nd}$ . The external forces are  $\mathbf{f} = (\sigma, \mathbf{0}) = (\sigma, \mathbf{0}, \mathbf{0})$ Since  $\mathbf{f}^d := \mathbf{f} - \mathbf{f}^{nd}$ 

$$\sigma^d := \sigma - \sigma^{nd} = \mathbf{0}$$
$$\mathbf{p}^d := \mathbf{0} - \mathbf{p}^{nd}$$

- Theoretical framework

- Comment on the notation used in classical textbooks

If moreover the Helmholtz energy depends on  $\varepsilon~$  and  $~\varepsilon^{p}$  only by

$$rac{1}{2}\left(arepsilon-arepsilon^{p}
ight):\mathbf{C}:\left(arepsilon-arepsilon^{p}
ight)$$

then  $-\tau^{nd} = \mathbf{C} : (\varepsilon - \varepsilon^p) = \sigma^{nd}$  hence

 $\tau^d = -\tau^{nd} = \sigma^{nd} = \sigma$ 

In classical textbooks f and g are functions of  $(\sigma, \mathbf{X})$ Actually the above relationships show that f and g are functions of the dissipative forces.

$$f = f\left(\tau^{d}, \mathbf{X}^{d}\right) = f\left(\sigma, \mathbf{X}\right), \quad g = g\left(\tau^{d}, \mathbf{X}^{d}\right) = g\left(\sigma, \mathbf{X}\right)$$

Constructive procedure

- Construction of a pseudo-potential

### Construction of a loading function

A plasticity model is defined by :

 $\mathbb{E} = \{\mathbf{x} \in \mathbb{V} \mid f(\mathbf{x}) \leq 0\}$  elastic domain for thermodynamic forces  $\nabla g(\mathbf{x})$  gives the direction of the flow  $\mathbf{x}^*$ . We define a loading function F as :

$$\forall (\mathbf{x}, \mathbf{y}) \in \mathbb{V} \times \mathbb{V}$$
  $F(\mathbf{x}, \mathbf{y}) := f(\mathbf{x}) + \nabla (g - f)(\mathbf{y}) \cdot (\mathbf{x} - \mathbf{y})$ 

$$abla_{\mathbf{x}}F(\mathbf{x},\mathbf{y}) = 
abla f(\mathbf{x}) + 
abla (g-f)(\mathbf{y})$$

Hence for  $\mathbf{x} = \mathbf{y}$  and for any  $\mathbf{y}$  :

Remark 1 : If  $\mathbf{x} = \mathbf{p}^{d'}$  and  $\mathbf{y} = -\mathbf{p}^{nd'}$  then  $\mathbf{p}^{d'} + \mathbf{p}^{nd'} = \mathbf{x} - \mathbf{y} = 0$ Remark 2 : For any  $\mathbf{y}$  the function  $F(\mathbf{x}, \mathbf{y}) := f(\mathbf{x}) + \nabla (g - f) (\mathbf{y}) \cdot (\mathbf{x} - \mathbf{y})$  is the sum of  $f(\mathbf{x})$  and of a linear function of  $\mathbf{x}$  hence F is convex in  $\mathbf{x}$ .

Constructive procedure

Construction of a pseudo-potential

## Construction of pseudo-potentials

$$\begin{split} \mathbb{E}_{\mathbf{y}} &= \{\mathbf{x} \in \mathbb{V} \ / \quad F(\mathbf{x}, \mathbf{y}) \leq 0\} \quad \text{ convex} \\ \phi\left(\mathbf{x}, \mathbf{y}\right) &:= \mathbb{I}_{\mathbb{E}_{\mathbf{y}}}(\mathbf{x}) \quad \text{ the indicator function of } \mathbf{E}_{\mathbf{y}} \end{split}$$

 $\phi^*(\mathbf{x}^*,\mathbf{y}) := \sup_{\mathbf{x} \in \mathbb{V}} (\mathbf{x} \cdot \mathbf{x}^* - \phi(\mathbf{x},\mathbf{y})) \quad \text{the Legendre-Fenchel conjugate of } \phi$ 

For any  $\mathbf{y}$ ,  $\phi^*(\mathbf{x}^*, \mathbf{y})$  is conjugate of an indicator function of a convex domain and it is also a convex function and for any  $\mathbf{y}$  it is positively homogenous with respect to  $\mathbf{x}^*$  and

 $\begin{array}{l} \forall \; (\mathbf{x},\mathbf{y},\mathbf{x}^*) \in \mathbb{V} \times \mathbb{V} \times \mathbb{V}^* \qquad \phi(\mathbf{x},\mathbf{y}) + \phi^*(\mathbf{x}^*,\mathbf{y}) \geq \mathbf{x} \cdot \mathbf{x}^* \\ \\ B(\mathbf{x},\mathbf{y},\mathbf{x}^*) := \phi(\mathbf{x},\mathbf{y}) + \phi^*(\mathbf{x}^*,\mathbf{y}) \end{array}$ 

The function B is bi-convex in  $\mathbf{x}$  and in  $\mathbf{x}^*$  and such that

$$\forall (\mathbf{x}, \mathbf{y}, \mathbf{x}^*) \in \mathbb{V} \times \mathbb{V} \times \mathbb{V}^* \qquad B(\mathbf{x}, \mathbf{y}, \mathbf{x}^*) \geq \mathbf{x} \cdot \mathbf{x}^*$$

- Constructive procedure

- Construction of a bipotentiel

## Construction of a bipotentiel

The dissipative forces associated to internal variables are opposite to the corresponding non-dissipative forces

$$\mathbf{p}^{d'} = -\mathbf{p}^{nd'} \Leftrightarrow \mathbf{x} = \mathbf{y}$$

#### Definition of a bipotential

For x = y ,B(x,x,x\*)defineabi - functionb(x,x\*) :

$$orall \; (\mathbf{x}, \mathbf{x}^*) \in \mathbb{V} imes \mathbb{V}^* \qquad b(\mathbf{x}, \mathbf{x}^*) := \phi(\mathbf{x}, \mathbf{x}) + \phi^*(\mathbf{x}^*, \mathbf{x})$$

The function b is bi-convex in  $\mathbf{x}$  and in  $\mathbf{x}^*$  and such that

$$orall (\mathbf{x}, \mathbf{x}^*) \in \mathbb{V} imes \mathbb{V}^* \qquad b(\mathbf{x}, \mathbf{x}^*) \geq \mathbf{x} \cdot \mathbf{x}^*$$

So there exists a couple  $(\tilde{\mathbf{x}}, \tilde{\mathbf{x}}^*)$  such that  $b(\tilde{\mathbf{x}}, \tilde{\mathbf{x}}^*) = \tilde{\mathbf{x}} \cdot \tilde{\mathbf{x}}^*$ 

Drucker-Prager model Non-associative elasto-perfectly plastic model :  $(\varepsilon, \mathbf{u}) = (\varepsilon, \varepsilon^p)$  state variables  $(\sigma^d, \mathbf{p}^d) = (\sigma^d, \tau^d)$  thermodynamic forces

$$f(\sigma) = \frac{\|dev(\sigma)\|}{k_d} + \frac{tr(\sigma)}{3} \tan \varphi - c$$

$$tr\left(\dot{\varepsilon}^{p}\right) = \dot{\lambda} \tan \theta \quad \text{with} \quad 0 < \tan \theta < \tan \varphi$$
$$dev\left(\dot{\varepsilon}^{p}\right) = \dot{\lambda} \frac{1}{k_{d}} \frac{dev\left(\sigma\right)}{\|dev\left(\sigma\right)\|}$$
$$\dot{\lambda}f\left(\sigma\right) = 0, \quad \dot{\lambda} \ge 0, \quad f\left(\sigma\right) \le 0$$

$$\mathbf{p}^d = (tr(\tau^d), dev(\tau^d)),$$

$$f\left(\mathbf{p}^{d}\right) = \frac{\left\| dev\left(\tau^{d}\right) \right\|}{k_{d}} + \frac{tr(\tau^{d})}{3} \tan \varphi - c$$
$$g\left(\mathbf{p}^{d}\right) = \frac{\left\| dev\left(\tau^{d}\right) \right\|}{k_{d}} + \frac{tr(\tau^{d})}{3} \tan \theta$$
$$\nabla \left(g - f\right) \left(\mathbf{p}^{d}\right) = \left(\tan \theta - \tan \varphi; 0\right) \quad \text{constant}$$

## Loading function F

$$F\left(\mathbf{p}^{d'},\mathbf{y}\right) = f\left(\mathbf{p}^{d'}\right) + \left(\tan\theta - \tan\varphi\right)\left(tr(\mathbf{p}^{d'} - \mathbf{y})\right)$$
$$\dot{\mathbf{u}}_{y} \in \partial_{\mathbf{p}^{d}} \mathbb{I}_{\mathbb{E}_{y}}(\mathbf{p}^{d'})$$
$$\text{for} \quad \mathbf{p}^{d'} = \tau^{d'} = \mathbf{y}$$
$$tr\left(\dot{\varepsilon}^{p}\right) = \dot{\lambda}\left(\tan\varphi + \left(\tan\theta - \tan\varphi\right)\right)$$
$$dev\left(\dot{\varepsilon}^{p}\right) = \dot{\lambda}\frac{1}{k_{d}}\frac{dev(\tau^{d})}{\|dev(\tau^{d})\|}$$
$$\dot{\lambda}f\left(\mathbf{p}^{d}\right) \leq 0 = 0, \quad \dot{\lambda} \geq 0, \quad f\left(\mathbf{p}^{d}\right) \leq 0$$

#### **Pseudo-potentials**

$$\begin{split} \phi\left(\tau^{d},\mathbf{y}\right) &= \mathbb{I}_{F(\tau^{d},\mathbf{y})\leq 0}(\tau^{d})\\ \phi^{*}(\dot{\varepsilon}^{p},\mathbf{y}) &= \left(c - \frac{tr(\mathbf{y})}{3}\tan\varphi\right)k_{d} \left\|dev\left(\dot{\varepsilon}^{p}\right)\right\| + \mathbb{I}_{k_{d}}\tan\theta\|dev(\dot{\varepsilon}^{p})\|\leq tr(\dot{\varepsilon}^{p}) \end{split}$$

#### **Bipotential**

$$\begin{split} b\left(\dot{\varepsilon}^{p},\tau^{d}\right) &:= \phi^{*}\left(\dot{\varepsilon}^{p};\tau^{d}\right) + \phi\left(\tau^{d};\tau^{d}\right) \\ b &= \left(c - \frac{tr(\tau^{d})}{3}\left(\tan\varphi - \tan\theta\right)\right) \frac{1}{\tan\theta} tr\left(\dot{\varepsilon}^{p}\right) \\ &+ \mathbb{I}_{k_{d}}\tan\theta \|dev(\dot{\varepsilon}^{p})\| \leq tr(\dot{\varepsilon}^{p}) + \mathbb{I}_{f(\tau^{d}) \leq 0} \end{split}$$

#### Non-linear Kinematic Hardening :classical formulation

$$\begin{aligned} \sigma &= \mathbf{C} : (\varepsilon - \varepsilon^{p}), & \mathbf{X}^{d} = \mathbf{D} : (\varepsilon^{p} - \beta) \\ \dot{\varepsilon}^{p} &= \dot{\lambda} \frac{dev(\sigma - \mathbf{X}^{d})}{\|dev(\sigma - \mathbf{X}^{d})\|}, & \dot{\beta} &= \dot{\lambda}k\mathbf{X}^{d} \\ f\left(\sigma - \mathbf{X}^{d}\right) &= \left\|dev\left(\sigma - \mathbf{X}^{d}\right)\right\| - \sqrt{\frac{2}{3}}\sigma_{y}, \\ \dot{\lambda}f &= 0, \ \dot{\lambda} \geq 0, \ f \leq 0 \\ \frac{df}{dt} &= 0 \quad \longrightarrow \dot{\lambda} = \frac{\mathbf{n}:\mathbf{C}:\dot{\varepsilon}}{\mathbf{n}:\mathbf{C}:\mathbf{n}+\mathbf{n}:\mathbf{D}:\mathbf{n}-k \ \mathbf{n}:\mathbf{D}:\mathbf{X}^{d}} \end{aligned}$$

Often  $\alpha = \varepsilon^p - \beta$  is used instead of  $\beta$  (Chaboche). The force  $\mathbf{X}^d$  is associated with the kinematic hardening. Our formulation

$$\int f\left( au^{d},\mathbf{X}^{d}
ight) = \left\| extsf{dev}\left( au^{d}
ight) 
ight\| - ilde{\sigma}_{y} \quad extsf{with} \quad ilde{\sigma}_{y} = \sqrt{rac{2}{3}}\sigma_{y}$$

From yielding function and plastic potential to pseudo-potentials and bipotential : a constructive procedure Non-linear Kinematic Hardening (NLK)

An additional scalar variable  $\zeta$  can be added.  $\mathbf{v} = (\varepsilon, \mathbf{u}) = (\varepsilon, \varepsilon^{p}, \beta, \zeta)$ , state variables  $\Psi = \frac{1}{2} (\varepsilon - \varepsilon^{p}) : \mathbf{C} : (\varepsilon - \varepsilon^{p}) + \frac{1}{2} (\varepsilon^{p} - \beta) : \mathbf{D} : (\varepsilon^{p} - \beta)$ 

non-dissipative forces :

$$\begin{aligned} \sigma^{nd} &= \mathbf{C} : (\varepsilon - \varepsilon^{p}) \\ \tau^{nd} &= -\mathbf{C} : (\varepsilon - \varepsilon^{p}) + \mathbf{D} : (\varepsilon^{p} - \beta) \\ \mathbf{X}^{nd} &= -\mathbf{D} : (\varepsilon^{p} - \beta) \\ R^{nd} &= 0 \\ \mathbf{p}^{nd} &= (\tau^{nd}, \mathbf{X}^{nd}, R^{nd}) \end{aligned}$$

with  $\left(\tau^{d'}, \mathbf{X}^{d'}, R^{d'}\right) \in \mathbb{S}_{d}^{2} \times \mathbb{S}_{d}^{2} \times \mathbb{R}$ : 
$$\begin{split} & \left[ \begin{split} & \tilde{f}\left(\tau^{d'}, \mathbf{X}^{d'}, R^{d'}\right) = f\left(\tau^{d'}, \mathbf{X}^{d'}\right) + R^{d'} \\ & = \left\|\tau^{d'}\right\| - \tilde{\sigma}_{y} + R^{d'} \\ & \tilde{g} = \left\|\tau^{d'}\right\| - \tilde{\sigma}_{y} + \frac{1}{2}k \left\|\mathbf{X}^{d'}\right\|^{2} + R^{d'} \end{split} \end{split}$$
 From yielding function and plastic potential to pseudo-potentials and bipotential : a constructive procedure Non-linear Kinematic Hardening (NLK)

Hence

$$abla ( ilde{g} - ilde{f})\left( au^{d'}, \mathbf{X}^{d'}, R^{d'}
ight) = \left(egin{array}{c} 0 \\ k\mathbf{X}^{d'} \\ 0 \end{array}
ight)$$

Loading function F

$$F(\mathbf{x}, \mathbf{y}) = \tilde{f}(\mathbf{x}) + \nabla(\tilde{g} - \tilde{f})(\mathbf{y}) \cdot (\mathbf{x} - \mathbf{y})$$
  
with  $\mathbf{x} = \mathbf{p}^{d'}$  and  $\mathbf{y} = -\mathbf{p}^{nd'}$   
 $F(\mathbf{p}^{d'}, -\mathbf{p}^{nd'}) = \tilde{f}\left(\tau^{d'}, \mathbf{X}^{d'}, R^{d'}\right) - k.\mathbf{X}^{nd'} \cdot (\mathbf{X}^{d'} + \mathbf{X}^{nd'})$ 

Corresponding flow rule

$$\begin{split} \dot{\varepsilon}^{p} &= \dot{\lambda} \frac{1}{k} \frac{\tau^{d}}{\|\tau^{d}\|} \\ \dot{\beta} &= \dot{\lambda} k (-\mathbf{X}^{nd}) = \lambda k (-\mathbf{X}^{d}) \\ \dot{\zeta} &= \dot{\lambda} \\ \dot{\lambda} \tilde{f} \left(\tau^{d}, \mathbf{X}^{d}, R^{d}\right) \leq 0 = 0, \quad \dot{\lambda} \geq 0, \quad \tilde{f} \left(\tau^{d}, \mathbf{X}^{d}, R^{d}\right) \leq 0 \end{split}$$

From yielding function and plastic potential to pseudo-potentials and bipotential : a constructive procedure Non-linear Kinematic Hardening (NLK)



FIG.: Non-linear Kinematic Hardening .Variation of the elastic domain  $\mathbb{E}_{y}$ .

For endochronic theory, no elastic domain.

$$\sigma = \mathbf{C} : (\varepsilon - \varepsilon^p), \qquad \dot{\varepsilon}^p = \tilde{\beta} \, \operatorname{dev}(\sigma)\dot{\zeta}, \qquad \dot{\zeta} \ge 0 \quad \text{with } \tilde{\beta} = \frac{\beta}{2G}$$

 $\mathbf{v} = (\varepsilon, \mathbf{u}) = (\varepsilon, \varepsilon^{p}, \zeta)$  state variables, with  $\zeta$  the intrinsic time .

$$\Psi = rac{1}{2} \left( arepsilon - arepsilon^{p} 
ight) : \mathbf{C} : \left( arepsilon - arepsilon^{p} 
ight)$$

non-dissipative forces in  $\ \mathbb{S}^2\times\mathbb{S}^2\times\mathbb{R}$ 

$$\sigma^{nd} = \mathbf{C} : (\varepsilon - \varepsilon^{p})$$
  
$$\mathbf{p}^{nd} = (\tau^{nd}, R^{nd}) = (-\mathbf{C} : (\varepsilon - \varepsilon^{p}), 0)$$

dissipative forces in  $\mathbb{S}^2_d \times \mathbb{R}$ 

$$f( au^d, R^d) = R^d \ 
abla g( au^d, R^d) = igg( egin{array}{c} eta & dev( au^d) \ 1 \end{array} igg)$$

 $\sim$ 

$$F(\mathbf{x}, \mathbf{y}) = \tilde{f}(\mathbf{x}) + \nabla(\tilde{g} - \tilde{f})(\mathbf{y}) \cdot (\mathbf{x} - \mathbf{y})$$
  
with  $\mathbf{x} = \mathbf{p}^{d'}$  and  $\mathbf{y} = -\mathbf{p}^{nd'} = -\left(\tau^{nd'}, R^{nd'}\right) \in \mathbb{S}_d^2 \times \mathbb{R}$   
 $F\left(\mathbf{p}^{d'}, -\mathbf{p}^{nd'}\right) = \tilde{\beta}\left(\tau^{d'} : \left(-\tau^{nd'}\right) - \left\|\tau^{nd'}\right\|^2\right) + R^{d'} \le 0\}$ 

Hence

$$\begin{split} \dot{\varepsilon}^{p} &= \dot{\lambda} \; \tilde{\beta} \left( -dev(\tau^{nd'}) \right) \Big|_{\substack{\mathbf{y} = \mathbf{p}^{d} \\ \dot{\zeta} = \lambda}} \\ & \dot{\zeta} = \lambda \\ \text{with} \quad \mathbf{y} = -\mathbf{p}^{nd'} = \mathbf{p}^{d'} \quad F = 0 \text{ hence} \\ & \dot{\lambda}F \leq 0 \text{ and } F \leq 0 \; \dot{\lambda} \geq 0 \end{split}$$

only condition : non-negativity of  $\dot{\lambda}$  the intrinsic time increment.



FIG.: Endochronic theory .

a) Variation of  $\mathbb{D}_y$ , domain of pseudo-potentiel . b) Variation of  $\mathbb{E}_y$ .

**u** displacement of a point M with respect to a fixed plan rigid body.  $(u_n < 0 \text{ impossible}, u_n = 0 \text{ contact}, u_n > 0 \text{ no contact})$   $\dot{\mathbf{u}} = \dot{\mathbf{u}}_t + \dot{u}_n \mathbf{n}$  velocity  $\mathbf{r}^d = \mathbf{r}_t^d + \mathbf{r}_n^d \mathbf{n}$  dissipative reaction of the rigid plan it must remain in the convex  $K = \{r / ||\mathbf{r}_t|| \le \mu r_n\}$ Description of the model

$$f(\mathbf{r}^{d}) := \|\mathbf{r}_{t}^{d}\| - \mu r_{n}^{d}$$
$$\dot{\mathbf{u}} = \dot{\lambda} \nabla g(\mathbf{r}^{d}) \iff \begin{cases} \dot{\mathbf{u}}_{t} = \dot{\lambda} \frac{\mathbf{r}_{t}^{d}}{\|\mathbf{r}_{t}^{d}\|} \\ \dot{u}_{n} = 0 \end{cases}$$

since 
$$\nabla f(\mathbf{r}^d) = \begin{cases} \frac{\mathbf{r}_t^d}{\|\mathbf{r}_t^d\|} & \text{hence } \nabla(g-f)(\mathbf{r}^d) = \begin{cases} 0\\ \mu \end{cases}$$

### Loading function F

$$F\left(\mathbf{r}^{d'},\mathbf{y}\right) = f\left(\mathbf{r}^{d'}\right) + \nabla\left(g - f\right)\left(\mathbf{y}\right) \cdot \left(\mathbf{r}^{d'} - \mathbf{y}\right)$$
$$= \left\|\mathbf{r}_{t}^{d'}\right\| - \mu r_{n}^{d'} + \mu (r_{n}^{d'} - y_{n})$$
$$= \left\|\mathbf{r}_{t}^{d'}\right\| - \mu y_{n}$$

Since **y** should be replaced by  $\mathbf{r}^{d'}$  and since  $r_n^{d'} \ge 0$  then  $y_n \ge 0$ Pseudo- potentials

$$\begin{aligned} \phi(\mathbf{r}^{d'},\mathbf{y}) &= \mathbb{I}_{F \leq 0}(\mathbf{r}^{d'}) \\ \phi^*(\dot{\mathbf{u}}',\mathbf{y}) &= \mathbb{I}_{R^-}(\dot{u}'_n) + \mu y_n \|\dot{\mathbf{u}}'_t\| \end{aligned}$$

For  $\mathbf{y} = \mathbf{x} = \mathbf{r}^{d'}$  de Saxcé bipotential

$$b(\dot{\mathbf{u}}', \mathbf{r}^{d'}) = \phi^*(\dot{\mathbf{u}}', \mathbf{r}^{d'}) + \phi(\mathbf{r}^{d'}, \mathbf{r}^{d'}) \\ = \mathbb{I}_{R^-}(\dot{u}'_n) + \mu r_n^{d'} \|\dot{\mathbf{u}}'_t\| + \mathbb{I}_{\mathcal{K}}(\mathbf{r}^{d'})$$

## Constructive procedure

Our constructive procedure permits to construct a loading function and then the corresponding pseudo-potentials and a bipotential. Based on the distinction between dissipative and non dissipative thermodynamic forces and on their relationship. The method is illustrated by four examples :

- 1. non-associative Drucker-Prager model,
- 2. non-linear kinematic model,
- 3. Bouc-Wen endochronic theory,
- 4. unilateral-contact with dry friction,

The same sort of procedure can be used to define other rate-independent flow rules



Thank you for your attention Any questions ?

