

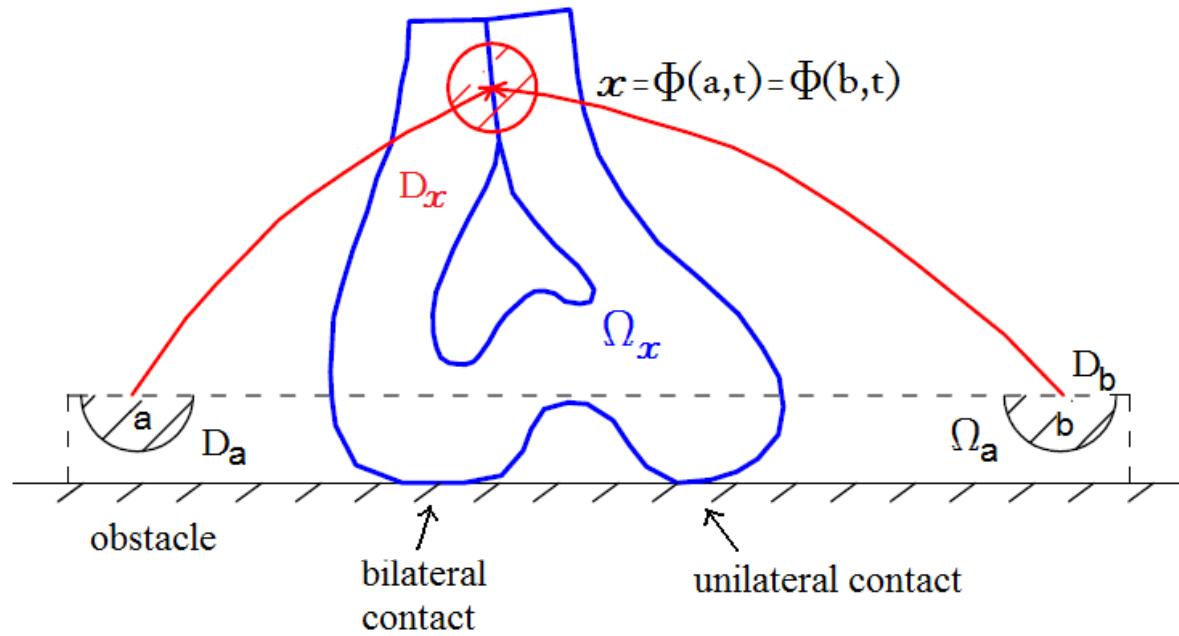


# Self-contact, self-collisions and large deformations

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$$x = \Phi(a, t) \quad x = (x_i) \quad a = (a_\alpha) = \Phi(a, 0)$$

$$\vec{U} = \frac{\partial \Phi}{\partial t} \quad \text{velocity}$$

$$F = \text{grad } \Phi = (F_{i\alpha}) = \frac{\partial \Phi_i}{\partial a_\alpha} \quad \text{gradient matrix}$$

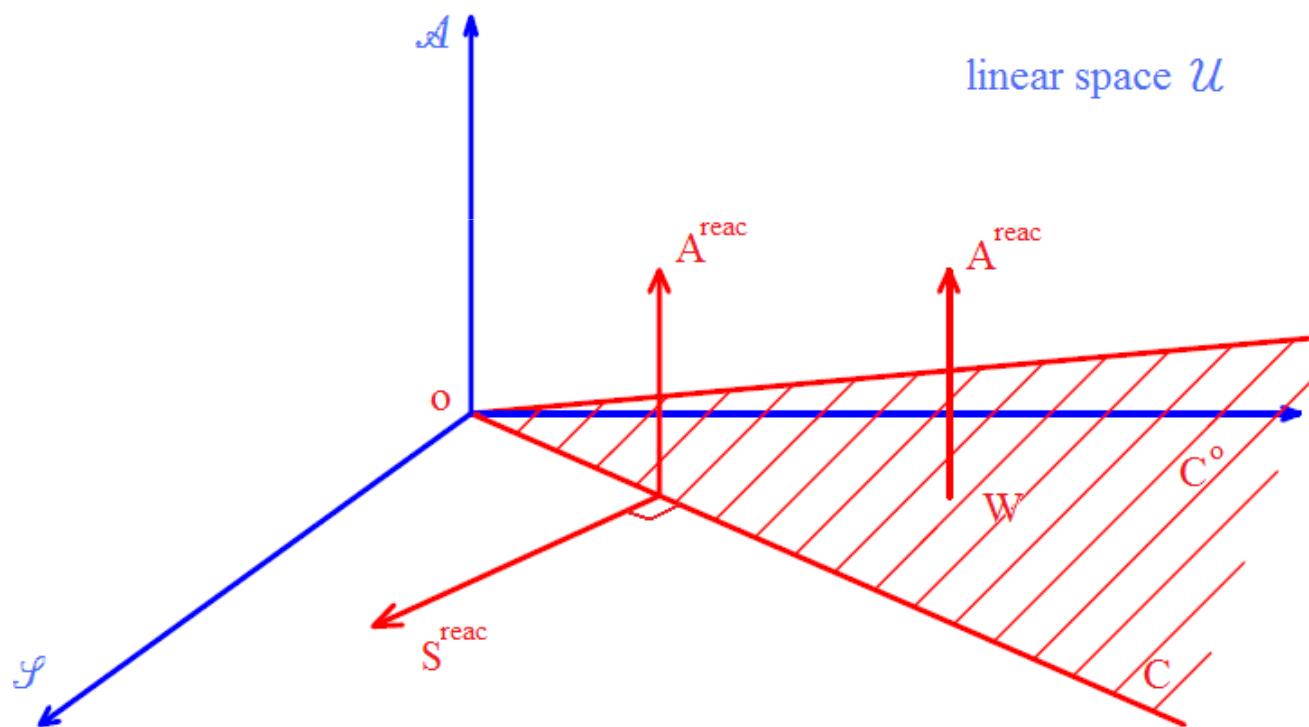
## 3x3 Matrices

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$$A : B = A_{ij} B_{ij}$$

$\begin{cases} \mathcal{S} & \text{symmetric matrices} \\ \mathcal{A} & \text{antisymmetric matrices} \end{cases}$ 
 $\mathcal{S} \perp \mathcal{A}$

$C = \{W \mid W \in \mathcal{S}; W \text{ is semidefinite positive}\}$  is a closed convex cone



$$F = RW, \quad W \in C, \quad RR^T = I, \quad \det R = 1$$

## Classical theory (Elastic behaviour)

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$$\Pi = \frac{\partial \psi}{\partial F}, \quad F = \text{grad } \Phi$$

$\Pi$  Boussinesq stress,  $\psi$  the free energy,  $\psi = \psi(F)$

$$\det F > 0$$

non interpenetration condition.

Rotation matrix R does not intervene; it is impossible that  $\psi$  is a convex function of F,

but

there exist mathematical results.

## How to take R into account?

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### VELOCITY OF DEFORMATION

$$grad \vec{U}$$

$$\Omega = \frac{\partial R}{\partial t} R^T$$

$$grad \Omega = \Omega_\alpha$$

### INTERNAL FORCE

$$\Pi$$

$$M \in \mathcal{A}$$

$$\Lambda = (\Lambda_\alpha)$$

### EQUATIONS OF MOTION

$$\rho \frac{\partial \vec{U}}{\partial t} = div \Pi \quad in \quad \Omega_a$$

$$div \Lambda + M = 0 \quad in \quad \Omega_a$$

+ B.C. + I.C.

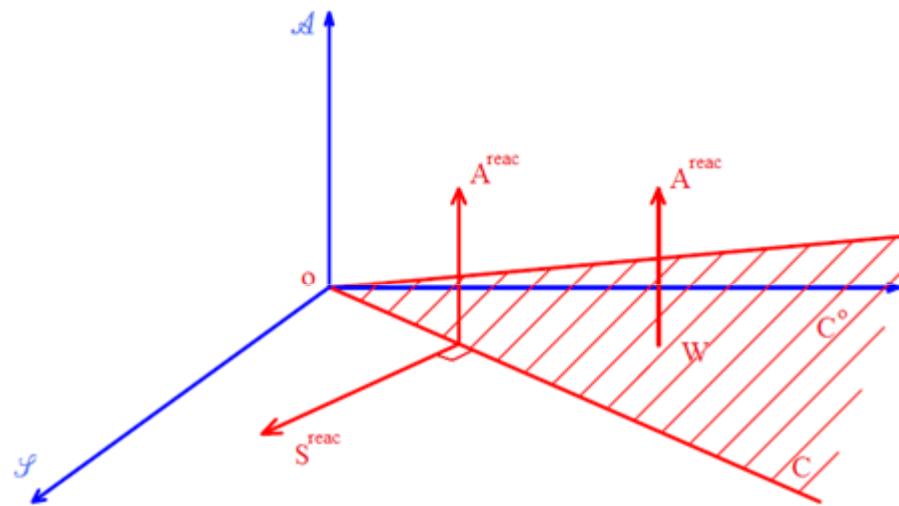
## Constitutive laws

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W is the physical quantity which describe the elongation.

### Impenetrability condition

$$W \in C$$



$\text{rank } W = 3 \longleftrightarrow$  no flattening

$\text{rank } W = 2 \longleftrightarrow$  flattening into a surface

$\text{rank } W = 1 \longleftrightarrow$  flattening into a curve

$\text{rank } W = 0 \longleftrightarrow$  flattening into a point

## Elastic constitutive laws

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grad R describes the spacial variation of the rotation matrix.

### Free energy

$$\overline{\Psi}(W, \text{grad}R) = \Psi(W, \|\text{grad}R\|^2) + I_c(W)$$

### Constitutive laws

$$\begin{cases} \Pi = R \left( \frac{\partial \Psi}{\partial W} + S^{\text{reac}} + A^{\text{reac}} \right) \\ S^{\text{reac}} \in \mathcal{S}, \quad A^{\text{reac}} \in \mathcal{A}, \quad S^{\text{reac}} + A^{\text{reac}} \in \partial I_c(W) \end{cases}$$

$$\Lambda = 4 \left( \frac{\partial \Psi}{\partial \|\text{grad}R\|^2} \right) (\text{grad}R) R^T$$

$$M = \Pi W R^T - R W \Pi^T$$

## In this theory

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- $(W, \text{grad}R) \rightarrow \Psi(W, \text{grad}R)$  may be convex.

The effect may be proportional to the cause.

- There exist non unique equilibrium positions in  $W^{1,p}(\Omega)$ ,  $p > 3$ .

- If  $\Psi(W) \rightarrow +\infty$  when  $\det W \rightarrow 0$  there is no flattening. Reaction  $A^{\text{reac}}$  is present.

- If  $\Psi(W) < +\infty$  for  $\det W = 0$  flattening is possible. Reaction  $A^{\text{reac}}$  and  $S^{\text{reac}}$  are present.

- Constitutive law

$$\Pi = \frac{\partial \Psi}{\partial F} = R \frac{\partial \Psi}{\partial W} \quad \text{is not always valid.}$$

$$\Pi \in R \left( \frac{\partial \Psi}{\partial W} + \partial I_c(W) \right) \quad \text{is always valid.}$$

## Self contact

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VELOCITY OF DEFORMATION

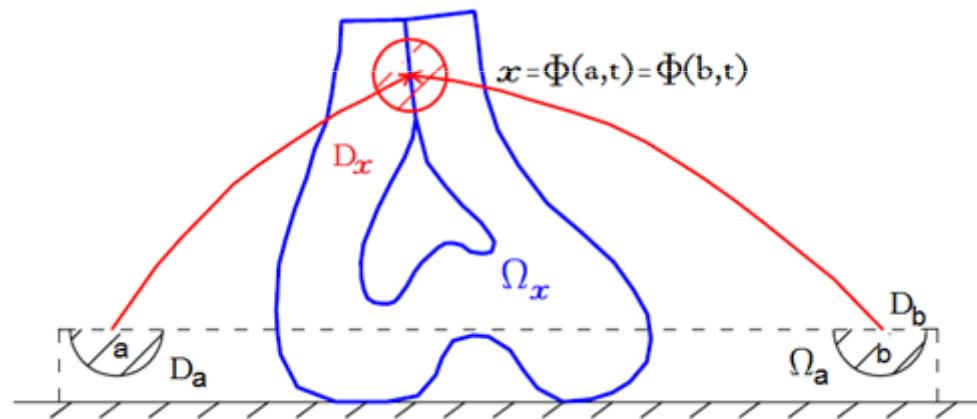
$$\vec{U}(a) \quad \vec{U}(b)$$

INTERNAL FORCE

$$\vec{R}(a) \quad \vec{R}(b)$$

EQUATIONS OF MOTION

$$\frac{\vec{R}(a)}{\|cof\ W(a)\|} + \frac{\vec{R}(b)}{\|cof\ W(b)\|} = 0$$



CONSTITUTIVE LAW

$$\vec{R} \in \partial \Phi (\vec{U}(a) - \vec{U}(b))$$

## Collisions

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### Self collisions

Interior forces become percussions

Constitutive laws involve

$$\frac{\vec{U}^+(a) - \vec{U}^+(b) + \vec{U}^-(a) - \vec{U}^-(b)}{2}$$

### Collisions when flattening

Boussinesq stress becomes Boussinesq percussion stress

No difficulty: velocity  $\vec{U}^+$  is uniquely given by velocity  $\vec{U}^-$

$$rank W = 3$$

*Unknowns*       $\Phi(a, t), R(a, t), A(a, t)$

$$\rho \frac{\partial^2 \Phi}{\partial t^2} = \operatorname{div} \left\{ R \left( \frac{\partial \Psi}{\partial W} + A \right) \right\}$$

$$\operatorname{grad} \Phi = R W(\Phi)$$

$$\operatorname{div} \left( \frac{\partial \Psi}{\partial \operatorname{grad} R} R^T \right) + R(AW(\Phi) + W(\Phi)A)R^T = 0$$

+ B.C. + I.C.

$A$  is the antisymmetric reaction matrix

$$A \in \partial I_c(W)$$

## A schematic example

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$$\Psi(W, \text{grad}R) = \frac{k}{2}(W - I)^2 + \frac{\hat{k}}{2}\|\text{grad}R\|^2 + I_C(W)$$

$$\rho \frac{\partial^2 \Phi}{\partial t^2} = \text{div} \{ R(k(W(\Phi) - I) + RA) \}$$

$$\text{grad } \Phi = R W(\Phi)$$

$$\text{div} \left( 4\hat{k}(\text{grad}R) R^T \right) + R(AW(\Phi) + W(\Phi)A)R^T = 0$$

$$\Pi \vec{N} = \vec{g}, \quad \Lambda \vec{N} = \vec{m} \quad \text{on } \Gamma_1$$

$$\Phi(a, t) = a, \quad R = I \quad \text{on } \Gamma_0$$

$$\Phi(a, 0) = a, \quad \frac{\partial \Phi}{\partial t}(a, 0) = 0$$

## A schematic example

Iterative method:  $\Phi^n$ ,  $R^n$ ,  $A^n$  are known at time  $n\Delta t$ .

**Step 1.**  $\rho \frac{\partial^2 \Phi}{\partial t^2} = \operatorname{div} \left\{ R^n (k(W(\Phi^n) - I) + R^n A^n) \right\}$

—————→ give  $\boxed{\Phi^{n+1}}$

**Step 2.**  $\operatorname{grad} \Phi^{n+1} = RW(\Phi^{n+1})$

—————→ give  $\boxed{R^{n+1}}$

**Step 3.**  $\operatorname{div} \left( 4\hat{k}(\operatorname{grad} R^{n+1}) R^{n+1T} \right) + R^{n+1} (AW(\Phi^{n+1}) + W(\Phi^{n+1})A) R^{n+1T} = 0$

—————→ give  $\boxed{A^{n+1}}$

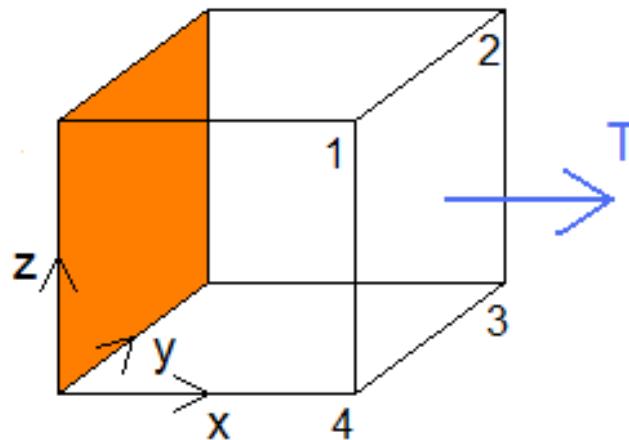
### Weak equations and finite elements

$\Phi$ ,  $R$  are piecewise continuous

$A$  is either piecewise continuous or piecewise constant

## Application 1 - Traction

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Only elongation  $\longrightarrow A = 0$  at each time step

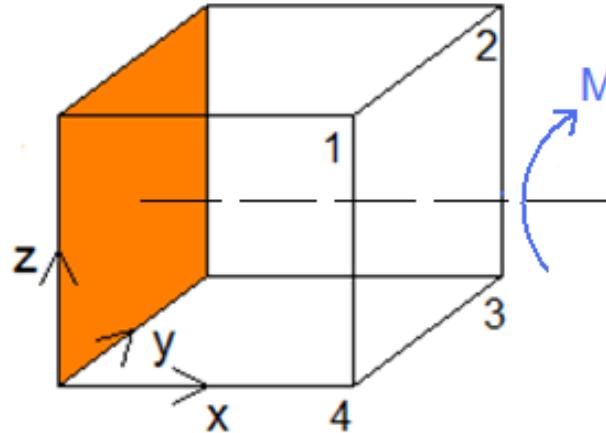
$R = I$  at each time step

$k$  is the elongation rigidity

Periodic motion

## Application 2 - Torque

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Only torsion  $\longrightarrow A \neq 0$  at each time step

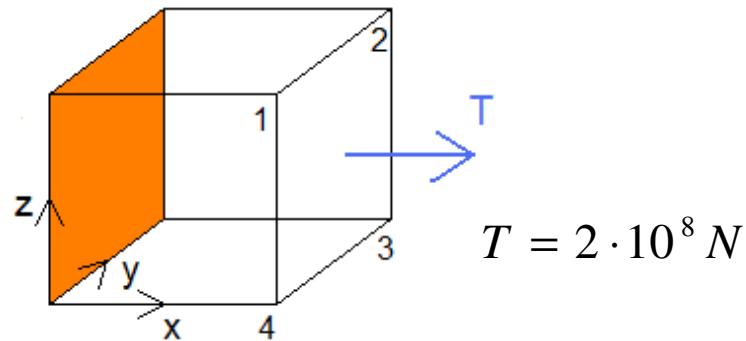
$R \neq I$  at each time step

$\hat{k}$  is the rotation rigidity.

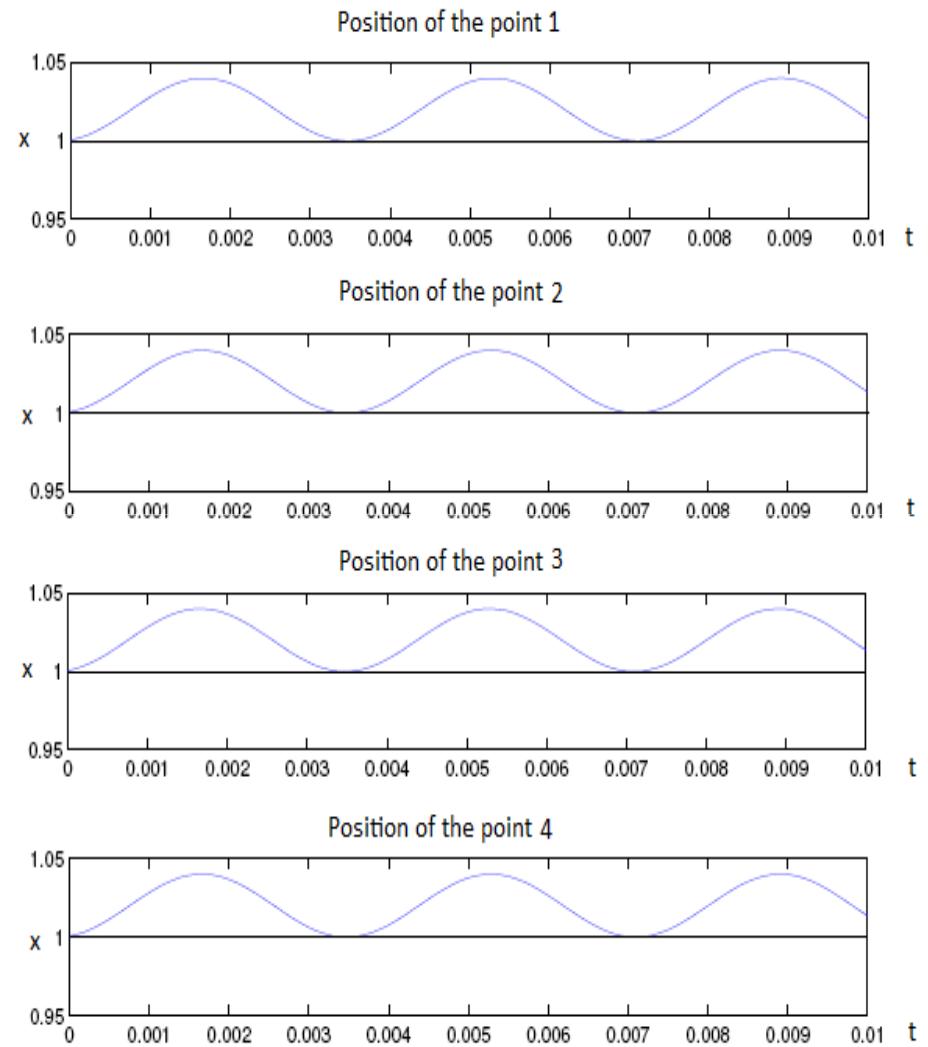
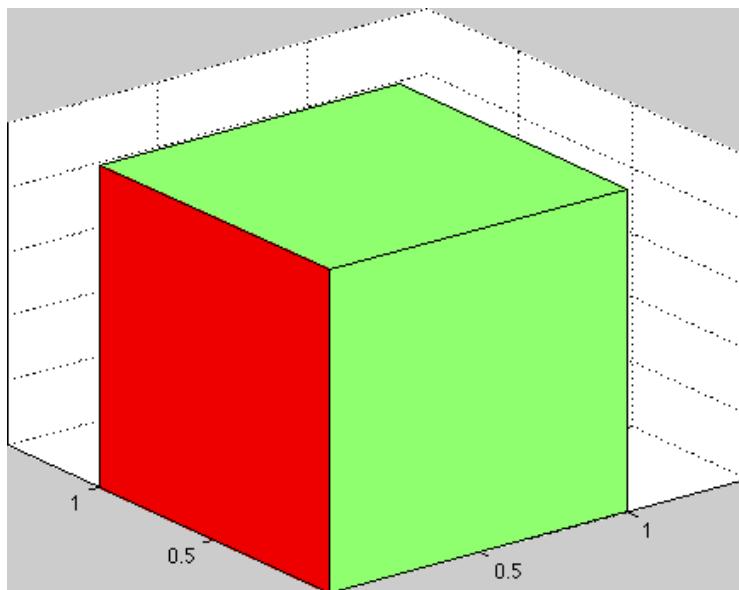
In case  $\hat{k} = 0$  (the usual theory) rotation does not have limitation.

Periodic motion

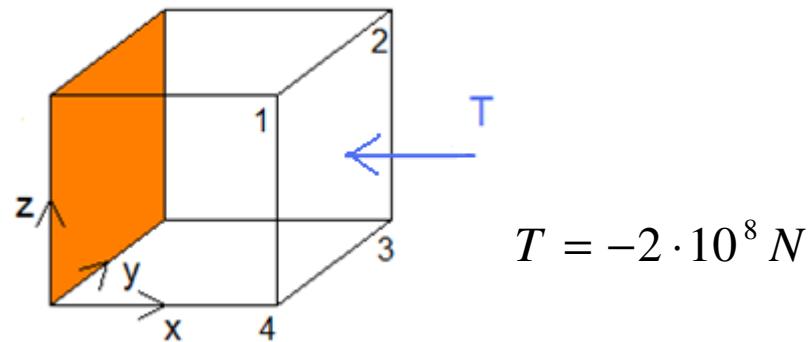
## Results



$$k = 1 \cdot 10^{10} \frac{N}{m^2} \quad \rho = 1 \cdot 10^3 \frac{kg}{m^3}$$



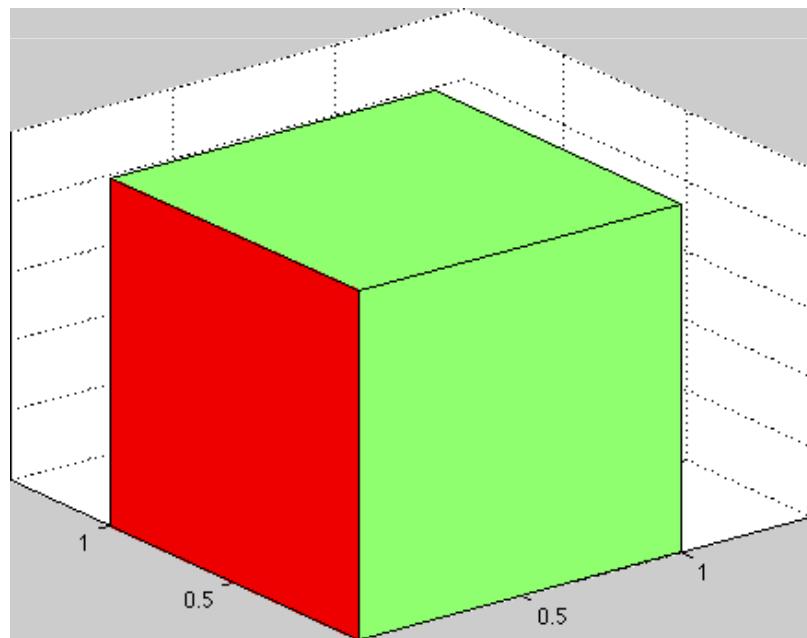
## Results



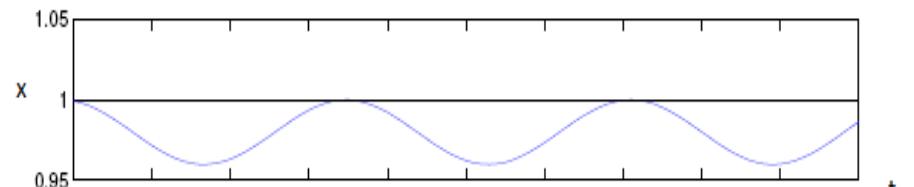
$$T = -2 \cdot 10^8 N$$

$$k = 1 \cdot 10^{10} \frac{N}{m^2}$$

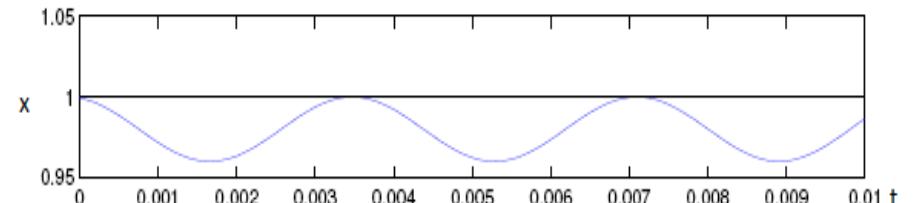
$$\rho = 1 \cdot 10^3 \frac{kg}{m^3}$$



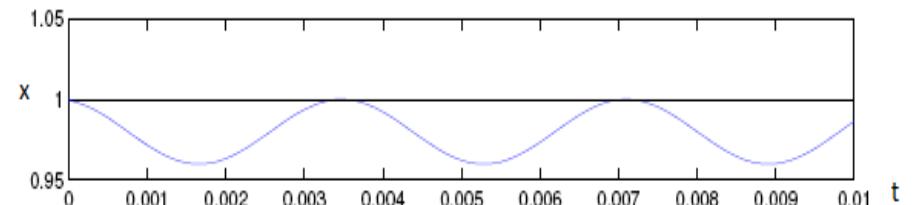
Position of the point 1



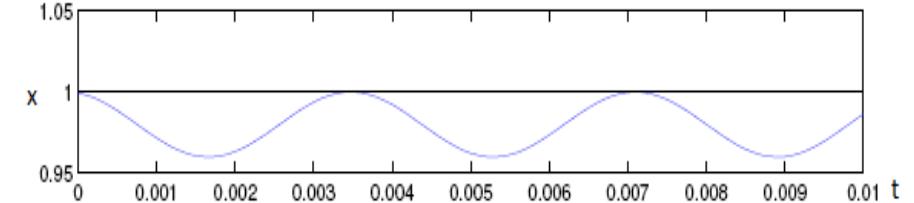
Position of the point 2



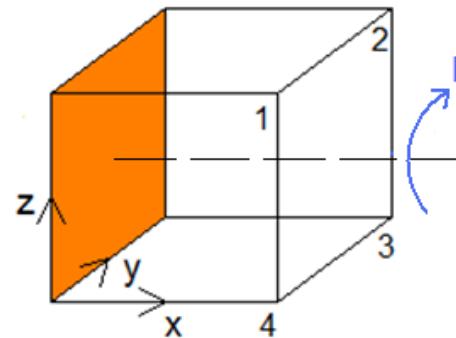
Position of the point 3



Position of the point 4



## Results

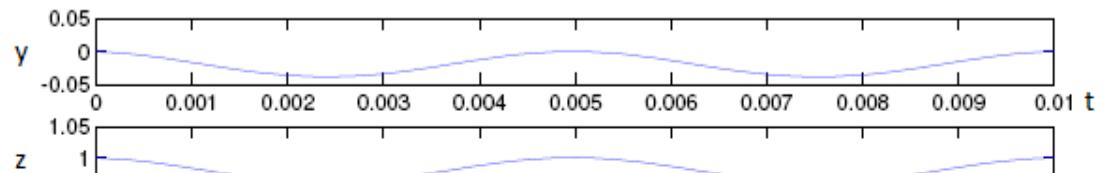


$$\hat{k} = 100$$

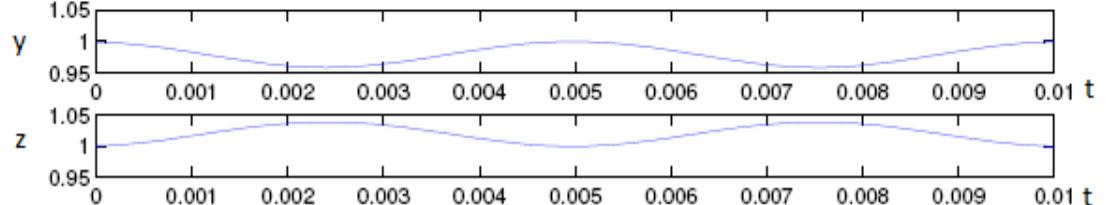
$$k = 1 \cdot 10^{10} \frac{N}{m^2} \quad \rho = 1 \cdot 10^3 \frac{N}{m^3}$$



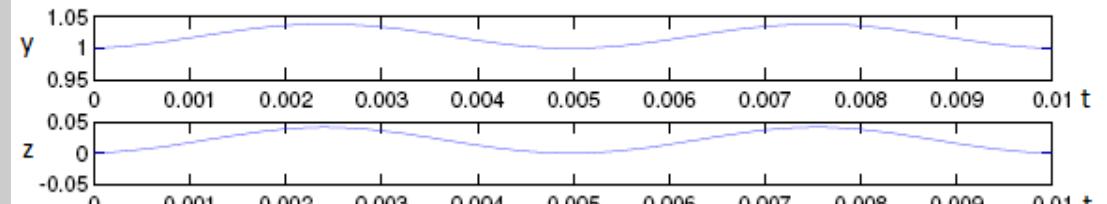
Position of the point 1



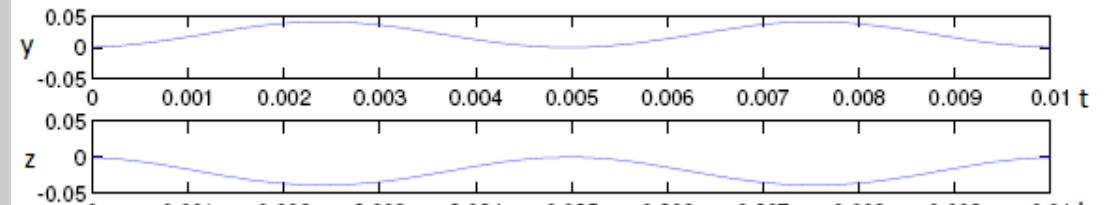
Position of the point 2



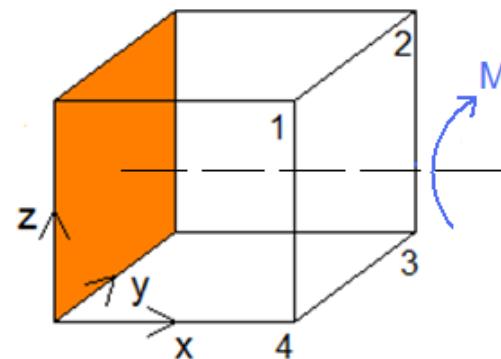
Position of the point 3



Position of the point 4



## Results



$$\hat{k} = 0$$

